IN-SITU OBSERVATION OF ErD₂ FORMATION DURING D₂ LOADING VIA NEUTRON DIFFRACTION

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ABSTRACT

In an effort to better understand the structural changes occurring during hydrogen loading of erbium target materials, we have performed in-situ D₂ loading of erbium metal (powder) at temperature (450°C) with simultaneous neutron diffraction analysis. This experiment tracked the conversion of Er metal to the α erbium deuteride (solid-solution) phase and then on to the β (flourite) phase. Complete conversion to ErD₂.0 was accomplished at 10 Torr D₂ pressure with deuterium fully occupying the tetrahedral sites in the fluorite lattice.

INTRODUCTION

Rare earth metals such as Er hold interest for hydrogen storage applications. The groundbreaking work on the Erbium-Hydrogen system by Lundin (1968) documents three possible phases (α, β, γ) for this metal hydride. The α phase can be understood as having the same hexagonal symmetry as that of Er metal, but with the addition of hydrogen into the host Er lattice as a solid solution. The β phase has a fluorite-type structure and usually occurs near the formula ErH₂, hence it is also referred to as the dihydride phase. Lundin (1968) also documents a tri-hydride phase (γ) which has also been recently explored by Tewell & King (2006). As our interest in this study was monitoring of the formation of ErD₂ from Er metal, we shall limit discussion in this report to the α and β phases.

Synthesis of the β phase via systems such as a Pressure-Composition-Temperature (PCT) apparatus (Ferriz, et al., 2007) results in powders and films that traverse the phase diagram for the erbium-hydride system. However, many of the synthesis protocols are based on empirical observations of the final synthesized compounds and little is understood regarding the crystallographic behavior of the α and β phase during hydrogen (i.e. protium, deuterium, and/or tritium) loading. As a means to probe the α and β phase while they are forming, we have undertaken in-situ deuterium loading with simultaneous neutron scattering. We loaded Er using D₂ gas as the scattering length for deuterium (6.671 fm) is of the same order as that of the Er species (7.79 fm), which means that a neutron scattering measurement will give nearly equal sensitivity to the two atomic species, opening up opportunities to monitor structural parameters such as site occupancy of the deuterium atoms within the α and β phases. We present here the
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details of the experimental setup for such an in-situ measurement and document the conversion of Er to ErD₂ via this technique.

EXPERIMENTAL

High purity (99.99%) Er metal was milled into chunks (size range of 100 μm to 2 mm) via cryogrinding. We chose to employ a powder specimen because a random neutron scattering of a loose powder provides a more straightforward analysis of the neutron diffraction datasets. No attempt was made to isolate the Er powder from the air atmosphere prior to loading it into the reaction vessel. Therefore, the Er undoubtedly contained the typical oxide passivation layer on the surface of the individual chunks of the powder sample. Because of the large grain size of the powder specimen, the surface-to-volume ratio is dominated by the bulk interior of the Er metal grains; the oxygen in the thin (~60 Å) passivation layer is very small in comparison to the bulk Er and is considered negligible for this experiment.

Figure 1. Schematic of the experimental setup for in-situ D₂ loading of Er metal.

The schematic of the experimental setup is shown in Figure 1. Vanadium is effectively transparent to neutrons; this metal was the logical choice for the heating element. Additionally, the heat shields for the heating element were fabricated from thin vanadium foil. A thermocouple (type K) was placed down into the reaction vessel to measure the temperature of the sample during heating. The thermocouple was placed about 1 mm above the powder Er sample. The gas system employed a roughing pump/turbo pump system that could obtain vacuum conditions of < 10⁻⁷ Torr throughout the entire gas system. The gas system also employed an isolation valve between the in-situ reactor chamber and the vacuum. This allowed
isolation of the system so that various D$_2$ gas pressures could be applied to the sample in the reactor chamber. Addition of D$_2$ gas into the reactor was controlled by a small needle valve plumbed in-line between the D$_2$ cylinder and the in-situ reactor. MKS Baratron pressure gauges were employed to monitor the D$_2$ pressures applied to the in-situ reactor.

Figure 2 shows the actual setup of the reactor vessel, gas system, and heater prior to installation into the experimental chamber of the High Intensity Powder Diffraction (HIPD) beam-line at LANSCE. A close-up view of the reactor chamber is shown as well. The actual reactor vessel was fabricated from fused silica (~7 mm diameter). The reactor vessel was attached to a vacuum flange by a glass-to-metal seal. The flange was subsequently attached to the upper part of the gas system. The entire gas system could be adjusted up-and-down by a gasket at the top plate of the setup. This enabled height adjustment for optimal placement of the specimen in the neutron beam.

Figure 3 shows the entire experimental setup installed into the chamber at HIPD ready for neutron diffraction analysis. The large neutron scattering chamber (approx. 1 m$^3$) of HIPD is typically evacuated to ~10$^{-5}$ Torr in order to reduce scatter and improve counting statistics during data collection. The vacuum conditions of the scattering chamber allowed straightforward use of the vanadium heating element without the concern for oxidation of the vanadium metal during heating for temperature values up to 700°C. Because the fused silica reactor vessel would experience various pressures on the internal walls of the reactor while simultaneously experiencing vacuum conditions of the neutron scattering chamber on the exterior reactor walls,
a trial run was performed without the use of D₂ gas. This was accomplished by simply heating the empty reactor vessel within the large HIPD chamber pumped to 10⁻⁵ Torr and maintaining atmospheric pressure (air) in the reactor and subsequent attached plumbing system. Cycling of air and vacuum conditions inside the heated reactor (300-700°C) showed that the fused silica reactor was robust and easily handled pressure cycling. As our experiment did not plan to exceed 500 Torr D₂ pressures, testing to atmospheric pressure (i.e. ~ 600 Torr for Los Alamos, NM) was sufficient to establish functionality of the reactor under conditions expected during loading.

Figure 3. Actual experimental setup on the HIPD beam-line at LANSCE.

Three sets of detector banks (40°, 90°, and 153°) served to obtain diffraction spectra from the sample. Note that because this is a time-of-flight (TOF) experiment, the specimen and detector banks are fixed. This significantly reduces complications of in-situ data collection with respect to specimen and detector alignment. The lower angle (40°) banks have higher intensity with moderate resolution over a large range of d-spacing. The higher angle banks (153°) have better resolution but a more limited range of d-spacing and lower intensity. The 90° banks are intermediate in resolution and d-spacing range, as compared to the 40° and 153° banks, while still yielding good intensity. All detector banks were used in the analysis. Diffraction data were refined using the program GSAS (Larson & Von Dreele, 2000; Toby, 2001).
RESULTS AND DISCUSSION

Histograms shown in Figure 4 demonstrate the excellent refinement of experimental data. As one can see, the solid green line calculated from the structural model matches well to the observed patterns (plotted in red as individual + symbols). Note that a region in the 90° and 40° banks was removed due to scatter from the Silica reaction vessel. Otherwise, the patterns were free of experimental artifacts. Excellent residual error values ($R_p < 5\%$) were typical for our analysis, indicating the appropriateness of the structural models employed in the refinement. The difference patterns, shown at the bottom of each plot (pink), are also employed as a visual gauge for the quality of the fit; in these refinements the difference patterns were essentially flat. This suggests appropriate modeling of the observed histograms. This also lends credibility to the resulting refined parameters.

Figure 4. Rietveld refinement of experimental histograms from 40°, 90°, and 153° detector banks. See text for details.

To obtain an overall picture of the hydration process, a contour map was generated as shown in Figure 5. This plot (employing data from one of the 90° banks) represents the sequential plotting of histograms from the specimen at 450°C. The plot shows how the neutron diffraction pattern changes as various pressures of $D_2$ are bled in from the $D_2$ cylinder. At the onset of the experiment the Er powder was at vacuum conditions (~$10^{-7}$ Torr) and held steady at 450°C. The histogram for Er is plotted at the bottom of the contour plot and is denoted by the label: no $D_2$. The hexagonal Er structure has its major peak (101) at ~2.7 Å as shown by the yellow band along the x-axis in the contour plot (yellow = high intensity, red = low intensity for contour.
Over the course of about 20 hours D\textsubscript{2} gas was allowed to flow into the reaction vessel; first at 0.1 Torr, then 1.0 Torr, and finally 10 Torr and above.

The contour plot shows how the Er pattern slowly expands (peaks shift to larger d-spacings) as deuterium is added into the reactor vessel. Initially, our observations at 0.1 Torr indicated the formation of only the $\alpha$ phase solid-solution. Saw, et al., (1983) have shown that the $\alpha$ phase for Scandium metal has the same structure as the rare-earth metal, but with deuterium locating in the interstitial sites of the hexagonal lattice. We observe this same phenomenon with our Er specimen. The $\alpha$ phase formation is indicated by shifting of the hexagonal peaks, but not the loss of any observed $hkl$ indices. With time, the specimen entered a two phase region of $\alpha$ phase along with the formation of the $\beta$ (fluorite) ErD\textsubscript{2-x} phase. This is clearly distinguished by the growth of the (111) peak of the $\beta$ phase at ~3.0 Å d-spacing. This peak is detectable roughly halfway through the 0.1 Torr exposure and grows dramatically with increased D\textsubscript{2} pressures. As the reaction continued to progress with time and increased D\textsubscript{2} pressure, the $\beta$ phase became the dominant phase fraction, until the sample fully converted to the ErD\textsubscript{2} fluorite as indicated by the strong (220) peak at ~1.8 Å as well as the (200) and (111) reflections as labeled at the top of the contour plot. We did not detect the presence of Er\textsubscript{2}O\textsubscript{3} in the observed diffraction data. As mentioned earlier, the Er metal most assuredly contained an oxide passivation layer due to exposure of the metal to air. The lack of detection of Er\textsubscript{2}O\textsubscript{3} would indicate that the passivation layer contributes an insignificant fraction of the measured intensity.

![Contour plot illustrating in-situ formation of the $\alpha$ and $\beta$ phases of erbium deuteride via D\textsubscript{2} loading at various pressures. Sample held at 450°C during D\textsubscript{2} loading. Red = low intensity, yellow = high intensity.](image-url)
Significant quantification of results could be obtained via Rietveld refinement. Table 1 documents various refined parameters for the $\alpha$ and $\beta$ phases during loading. We document our results as a function of Run Number for purposes of bookkeeping and comparison of the progression of the reaction. However, the Run Number can be roughly translated as time where typical histogram collection runs required roughly 20 to 40 minutes. We show the phase fraction (wt %) of the $\alpha$ and $\beta$ phases as a function of Run Number in Figure 6. In this plot the regions are highlighted based on the existing $D_2$ pressure present on the powder during each Run. The plot shows that the $\beta$ phase becomes the majority phase in the reactor even at 0.1 Torr.

### Table 1. Refined parameters for $\alpha$ and $\beta$ phases during $D_2$ loading at 450°C.

<table>
<thead>
<tr>
<th>Run #</th>
<th>$P_{D_2}$ (Torr)</th>
<th>Wt % $\alpha$ phase</th>
<th>a axis (Å)</th>
<th>c axis (Å)</th>
<th>cell vol. ($Å^3$)</th>
<th>Wt % $\beta$ phase</th>
<th>a axis (Å)</th>
<th>cell vol. ($Å^3$)</th>
<th>Rp (%)</th>
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*Er metal under vacuum prior to exposure to $D_2$ gas

Parentheses next to numbers indicate 3σ error on the last digit of value

Figure 6. Weight fraction of $\alpha$ and $\beta$ phases vs. Run Number for $D_2$ loading at 450°C.
The setting of the D$_2$ pressure during analysis was typically performed by adjusting a needle valve controlling the D$_2$ gas until the pressure of the reactor read the desired D$_2$ loading pressure on the MKS Baratron readout. This pressure value tended to decrease over time as the D$_2$ gas was consumed by the Er powder in the reactor. Hence, the experiment required monitoring of the D$_2$ pressure and recurrent adjustments of the needle valve to keep the pressure near to its set-point. We chose to increase pressure to 1.0 Torr between run 3560 and 3561 because we had reached conditions where the D$_2$ gas pressure of 0.1 Torr stabilized over the Er powder. This may not have been a true thermodynamic equilibrium condition for the sample, as perhaps with more time the sample might have converted fully to ErD$_2$. However, at this point in our experiment it made sense to increase the D$_2$ pressure so that conversion to the $\beta$ phase could be achieved in the limited time frame of the experimental beam-time.

Upon increase to 1.0 Torr, the conversion to $\beta$ phase continued to progress with complete conversion to ErD$_2$ occurring at ~10 Torr D$_2$ (not shown on plot). Table 1 shows the refined lattice parameters for both the $\alpha$ and $\beta$ phases, and one can see the dramatic change of hexagonal lattice with deuterium exposure. In contrast, the $\beta$ phase shows very little variation in lattice parameter upon formation within the two-phase region as well as when fully converted to ErD$_2$ at 10 Torr. Refinements of site occupancy for fully converted $\beta$ phase indicated essentially full tetrahedral (8c) deuterium sites at (1/4 1/4 1/4) for space group Fm-3m (225). This suggests that the $\beta$ phase forms with near stoichiometric fluorite composition even at small phase fractions within the two-phase region. Udovic, et al., (1994) demonstrated possible location of hydrogen in the octahedral (4b) sites of the $\beta$-TbH$_{2+x}$ phase. We did not detect significant deuterium occupancy in the octahedral sites for D$_2$ pressures $\leq$ 10 Torr. However, subsequent overpressures did indicate partial occupancy of the octahedral sites. Overpressure studies will be discussed in a later publication.

CONCLUSIONS

In-situ neutron diffraction yielded structural information regarding deuterium loading for Er metal at 450°C. The $\alpha$ phase shows dramatic cell expansion upon exposure to D$_2$. The $\beta$ phase shows little structural change in the ($\alpha + \beta$) two-phase region. This suggests formation of the $\beta$ phase near ErD$_2$ stoichiometry. No significant octahedral-site occupation was detected for deuterium in the $\beta$ phase at 450°C for D$_2$ pressures $\leq$ 10 Torr.

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